Introduction on Reduced Order Methods in CFD: State of the art and Perspectives



Leading Motivation: Computational Sciences challenges

- **Reduced order modelling** is a quickly emerging field in applied mathematics and computational science and engineering.
- Present and future efforts: towards multiphysics problems, as well as coupled systems.
- Growing demand of
 - efficient computational tools for
 - * many query and real time computations,
 - * parametric formulations,
 - * simulations of increasingly complex systems with uncertain scenarios,

by industrial and clinical research partners.

 The need of a computational collaboration rather than a competition between High Performance Computing (HPC) and Reduced Order Methods (ROM), as well as Full/High Order and Reduced Order Methods.



Overview

our current efforts, aims and perspectives at SISSA mathLab A team developing Advanced Reduced Order Methods for parametric PDEs with a special focus on Computational Fluid Dynamics



Overview:

our current efforts, aims and perspectives at SISSA mathLab

A team developing Advanced Reduced Order Methods with special focus on Computational Fluid Dynamics:

- to face and overcome several limitations of the state of the art for parametric ROM in CFD;
- to improve capabilities of reduced order methodologies for more demanding applications in industrial, medical and applied sciences settings;
- to carry out important methodological developments in Numerical Analysis, with special emphasis on mathematical modelling and a more extensive exploitation of Computational Science and Engineering;
- focus on Computational Fluid Dynamics as a central topic to enhance broader applications in multiphysics and coupled settings, as well as more realistic models (e.g. aeronautical, mechanical, naval, off-shore, wind, sport, biomedical engineering and also cardiovascular surgery planning).



Overview of the physical problems

The interest is in viscous parametrized incompressible flows Industrial Flows



Naval Eng.



Aeronautics Biomedical Applications



Industrial App.







Possible applications can be found in naval and nautical engineering, aeronautical engineering and industrial engineering.

In general any application dealing with incompressible fluid dynamic problems that has the response depending on parameter changes (Reynolds Number, Grashof Number, Geometrical parameters ..)

Overview: our current efforts, aims and perspectives

• Towards Real-Time Computing and Visualization, through an Offline–Online computational paradigm that combines

High Performance to Computing Advanced Reduced Order Modelling techniques.

In situ, tablets or smartphones, real time



HPC facilities, time demanding

"Science" driven



[&]quot;Industrial needs" driven

- Export numerical simulations and scientific computing in fields and places where at the state of the art there is still little exploitation.
- Development of new open-source tools based on reduced order methods:
 - ITHACA, In real Time Highly Advanced Computational Applications, as an add-on to integrate already well established CSE/CFD open-source software libraries (FV, SEM) with ROMs (OpenFoam, Nektar, FEniCS, Libmesh)
 - * RBniCS as educational initiative (FEM) for newcomer ROM users (training).
 - * Argos Advanced Reduced order modellinG Online computational web server for parametric Systems
 - * ATLAS



http://mathlab.sissa.it/cse-software

Intrusive Reduced Order Methods in a nutshell

- () $^{\mathcal{N}}$: "truth" full order method (FEM, FV, FD, SEM) to be accelerated
- ()_N: reduced order method (ROM) the accelerator
- * Input parameters:

 μ (geometry, physical properties, etc.)

* Parametrized PDE:

$$\mathcal{A}(u(\mu);\mu) = 0 \quad \rightsquigarrow \quad \mathbf{A}^{\mathcal{N}}(\mu)\mathbf{u}^{\mathcal{N}}(\mu) = 0 \quad \rightsquigarrow \quad \mathbf{A}_{\mathcal{N}}(\mu)\mathbf{u}_{\mathcal{N}}(\mu) = 0$$
reduced order

* Output:

$$egin{array}{rll} s(\mu) &pprox & s^{\mathcal{N}}(\mu) &pprox & s_{\mathcal{N}}(\mu) \ & ext{full order} & ext{reduced order} \end{array}$$

* Input-Output evaluation:

$$\mu \hspace{0.1in}
ightarrow \hspace{0.1in} s^{\mathcal{N}}(\mu) \hspace{0.1in}
ightarrow \hspace{0.1in} s_{\mathcal{N}}(\mu)$$

- Reduced Basis Method(RB): continuation method in non-linear structural mechanics...
- Proper Orthogonal Decomposition(POD): transient and turbulent flows...
- Other methodologies: Proper Generalized Decomposition (PGD), Hierarchical Model Reduction (HiMod).

J. S. Hesthaven, G. Rozza, B. Stamm. *Certified Reduced Basis Methods for Parametrized Partial Differential Equations*. SpringerBriefs in Mathematics. Springer, 2015

Intrusive Reduced Order Methods in a nutshell

- () $^{\mathcal{N}}$: "truth" full order method (FEM, FV, FD, SEM) to be accelerated
- ()_N: reduced order method (ROM) the accelerator
- Offline: very expensive preprocessing (full order): basis calculation (done once) after suitable parameters sampling (greedy, POD, ...)

$$\mathcal{Z}^{\mathsf{T}}$$

• Online: extremely fast (reduced order): real-time input-output evaluation $\mu \rightarrow s_N(\mu)$ thanks to an efficient assembly of problem operators

$$\mathbf{A}_{N}(\mu) = \sum_{q} \theta^{q}(\mu) \mathbf{A}_{N}^{q}, \text{ where } \mathbf{A}_{N}^{q} = \mathcal{Z}^{T} \mathbf{A}^{\mathcal{N},q} \mathcal{Z}$$
$$= \sum_{q} \theta^{q}(\mu) \mathbf{A}_{N}^{q} \text{ where } \mathbf{A}_{N}^{q} = \mathbf{\mathcal{Z}}^{T}$$
$$\mathbf{A}^{\mathcal{N},q} \mathcal{Z}$$

 Numerical issues: approximation stability, error bounds and stability factors, efficient (geometrical) parametrization, sampling, coupling, nonlinearities...

... reduction in parameter space

J. S. Hesthaven, G. Rozza, B. Stamm. *Certified Reduced Basis Methods for Parametrized Partial Differential Equations*. SpringerBriefs in Mathematics. Springer, 2015

G. Rozza ROM for PDEs

Overview on the topics: from intrusive to non-intrusive ROM

- ROMs exploit a parametrized formulation of the problem. In particular, an efficient geometrical parametrization is required when interested in the variation of the domain/interface, such as in shape optimization or fluid-structure interaction problems $\Omega_o(\mu) = T(\Omega; \mu).$
- Focus of this lecture: show some state of the art and perspectives in parametric flow problems treated in the reduced order context for
 - complex computational mechanics phenomena and bifurcations;
 - fluid-structure interaction (FSI) reduced problems;
 - flow control;
 - uncertainty quantification (UQ);
 - inverse problems;
 - shape optimization;
 - and some perspectives and challenges.



Shape parameterization for ROM

- Free-Form Deformations (FFD) [Lassila, Rozza, CMAME, 2010], [Salmoiraghi et al., AMSES, 2016].
- Radial Basis Functions (RBF) [Manzoni et al., IJNMBE, 2011].
- Transfinite Mapping (TM) [Løvgren, Maday, Rønquist, 2006], [lapichino *et al.*, CMAME, 2012].
- Vascular shape parametrization [Ballarin *et al.*, JCP, 2016].
- Reduced inverse Distance Weighting [D'Amario et al, 2017].



#CFD #intrusive #ROM

ROM and stability for fluid mechanics problems with Francesco Ballarin, Giovanni Stabile, Shafqat Ali, Enrique Delgado





Reduced-order numerical simulations by POD-Galerkin ROM

- parametrized formulation of Navier-Stokes equations (modelling Newtonian fluid);
- offline stage:
 - intensive phase, on HPC architectures, to be done once;
 - Finite Element approximation of the problem for few values of the parameters (snapshots):

for
$$\mu \in \mathcal{D}$$
, find $(\underline{\mathbf{u}}^{\mathcal{N}}(\mu), \underline{\mathbf{p}}^{\mathcal{N}}(\mu)) \in \mathbb{R}^{\mathcal{N}_{\mathbf{u}}} \times \mathbb{R}^{\mathcal{N}_{p}}$, large \mathcal{N}

$$\begin{bmatrix} A^{\mathcal{N}}(\boldsymbol{\mu}) + C^{\mathcal{N}}(\underline{\mathbf{u}}^{\mathcal{N}}(\boldsymbol{\mu});\boldsymbol{\mu}) & B^{\mathcal{N}}(\boldsymbol{\mu})^{\mathsf{T}} \\ B^{\mathcal{N}}(\boldsymbol{\mu}) & O \end{bmatrix} \begin{bmatrix} \underline{\mathbf{u}}^{\mathcal{N}}(\boldsymbol{\mu}) \\ \underline{\mathbf{p}}^{\mathcal{N}}(\boldsymbol{\mu}) \end{bmatrix} = \begin{bmatrix} \underline{f}^{\mathcal{N}}(\boldsymbol{\mu}) \\ \underline{\mathbf{0}} \end{bmatrix}$$

• [POD] Proper Orthogonal Decomposition (based on singular value decomposition) to extract optimal basis functions from the set of numerical simulations (snapshots) of the system to build \mathcal{Z} . [RB] Greedy as an alternative.

Aubry et al. J. Fluid Mech. 1988; Ravindran, Int. J. Numer. Meth. Fluids, 2000

online stage

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 - Finite Element approximation of the problem for few values of the parameters (snapshots)
 - [POD] Proper Orthogonal Decomposition (based on singular value decomposition) to extract optimal basis functions from the set of numerical simulations (snapshots) of the system to build \mathcal{Z} .

Build the correlation matrices $\mathbf{C}^{\boldsymbol{\mu}}, \mathbf{C}^{\boldsymbol{\rho}} \in \mathbb{R}^{N_{train} \times N_{train}}$, where N_{train} is the dimension of the training set and

$$\mathbf{C}^{\boldsymbol{u}}_{ij} = (\underline{\boldsymbol{u}}^{\mathcal{N}}(\boldsymbol{\mu}_i), \underline{\boldsymbol{u}}^{\mathcal{N}}(\boldsymbol{\mu}_j)) \text{ and } \mathbf{C}^{\boldsymbol{p}}_{ij} = (\underline{\boldsymbol{p}}^{\mathcal{N}}(\boldsymbol{\mu}_i), \underline{\boldsymbol{p}}^{\mathcal{N}}(\boldsymbol{\mu}_j)) \quad i, j = 1, \dots, N_{train}.$$

Then we find (λ_i^u, v_i^u) and (λ_i^p, v_i^p) such that $\mathbf{C}^u v_i^u = \lambda_i^u v_i^u$ and $\mathbf{C}^p v_i^p = \lambda_i^p v_i^p$. We retain only the first N_u and N_p eigenvalues for pressure and velocity, respectively.

The reduced space is span $\{\Phi_1^{\boldsymbol{u}}, \ldots, \Phi_{N_{\boldsymbol{u}}}^{\boldsymbol{u}}, \Phi_1^{\boldsymbol{p}}, \ldots, \Phi_{N_{\boldsymbol{p}}}^{\boldsymbol{p}}\}$, where the basis function $\Phi_i^{\boldsymbol{u}}$ and $\Phi_i^{\boldsymbol{p}}$ are the eigenvectors of $\lambda_i^{\boldsymbol{u}}$ and $\lambda_i^{\boldsymbol{p}}$, respectively. Aubry et al. J. Fluid Mech. 1988; Ravindran, Int. J. Numer. Meth. Fluids. 2000

online stage

Reduced-order numerical simulations by POD-Galerkin ROM

- parametrized formulation of Navier-Stokes equations (modelling Newtonian fluid);
- offline stage
- online stage:
 - inexpensive and very fast, on a laptop, to be done multiple times (for each new value of the parameters);
 - $\circ~$ Galerkin projection over a reduced basis space:

for
$$\mu \in \mathcal{D}$$
, find $(\underline{\mathbf{u}}_{\mathsf{N}}(\mu), \underline{\mathbf{p}}_{\mathsf{N}}(\mu)) \in \mathbb{R}^{N_{\mathsf{u}}} imes \mathbb{R}^{N_{\mathsf{p}}}$, $\boxed{N = N_{\mathsf{u}} + N_{\rho} \ll \mathcal{N}}$

$$\begin{bmatrix} A_{\mathsf{N}}(\mu) + C_{\mathsf{N}}(\underline{\mathbf{u}}_{\mathsf{N}}(\mu);\mu) & B_{\mathsf{N}}(\mu)^{\mathsf{T}} \\ B_{\mathsf{N}}(\mu) & O \end{bmatrix} \begin{bmatrix} \underline{\mathbf{u}}_{\mathsf{N}}(\mu) \\ \underline{\mathbf{p}}_{\mathsf{N}}(\mu) \end{bmatrix} = \begin{bmatrix} \underline{f}_{\mathsf{N}}(\mu) \\ \underline{\mathbf{0}} \end{bmatrix}$$

Inf-sup stabilization and pressure recovery

- inf-sup condition is not necessarily preserved by Galerkin projection in the online phase.
- reduced velocity space enrichment by supremizer solutions,

$$\begin{split} V_{N} &= \text{POD}(\{\boldsymbol{u}^{\mathcal{N}}(\boldsymbol{\mu}^{i})\}_{i=1}^{N_{\text{train}}}; N_{u}) \oplus \text{POD}(\{S^{\mu'} \boldsymbol{\rho}^{\mathcal{N}}(\boldsymbol{\mu}^{i})\}_{i=1}^{N_{\text{train}}}; N_{s}), \\ Q_{N} &= \text{POD}(\{\boldsymbol{\rho}^{\mathcal{N}}(\boldsymbol{\mu}^{i})\}_{i=1}^{N_{\text{train}}}; N_{\rho}), \end{split}$$

where $S^{\mu}: Q^{\mathcal{N}} \to V^{\mathcal{N}}$ is the **supremizer operator** given by

$$(S^{\mu}p^{\mathcal{N}}, w^{\mathcal{N}})_{V} = b(p^{\mathcal{N}}, w^{\mathcal{N}}; \mu), \quad \forall w \in V^{\mathcal{N}}.$$

where $b(\cdot, \cdot; \boldsymbol{\mu}) = \int_{\Omega} p \operatorname{div} \boldsymbol{w} d\Omega$ (pressure-divergence term) In order to fulfill an *inf-sup condition at the reduced-order level* to

$$\beta_N(\mu) = \inf_{\underline{\mathbf{q}}_N \neq \underline{\mathbf{0}}} \sup_{\underline{\mathbf{v}}_N \neq \underline{\mathbf{0}}} \frac{\underline{\mathbf{q}}_N^\top B_N(\mu) \underline{\mathbf{v}}_N}{\|\underline{\mathbf{v}}_N\| \mathbf{v}_N \| \underline{\mathbf{q}}_N \| \mathbf{q}_N} \geq \tilde{\beta}_N > 0 \qquad \forall \mu \in \mathcal{D}.$$

where $B_N(\mu)$ is the reduced-order matrix associated to the divergence term. (*Rozza, Veroy. CMAME, 2007, Rozza et al, Numerische Mathematik, 2013. Ballarin et al. IJNME, 2015*). Other options: residual-based stabilization procedures for POD-Galerkin (*Caiazzo, Iliescu et al. JCP, 2014*), Petrov-Galerkin (*Dahmen; Carlberg; Abdulle, Budac*), div-free approach (*Lovgren et al.*).

G. Rozza ROM for PDEs

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Some ROM challenges in CFD: to higher Reynolds parametrized flows

- ROMs of parametrized viscous flows for low and moderate Reynolds number are well developed: we need to increase Reynolds number for several industrial applications.
- Offline–Online stabilization techniques for parametrized flows (geometry, physics) is derived from streamline upwind Petrov-Galerkin (SUPG), . . .

 $\sup_{\mathbf{v}_N\neq 0}\frac{b(\mathbf{v}_N,q_N;\boldsymbol{\mu})}{\|\mathbf{v}_N\|_{V_N}}+s(q_N,q_N)^{\frac{1}{2}}\geq \tilde{\beta}_N\|q_N\|_{Q_N}>0, \ \forall q_N\in Q_N, \forall \boldsymbol{\mu}\in \mathcal{D} \ \text{(Generalized inf-sup)}.$

• A ROM variational multiscale approach in parametrized context towards turbulence modelling and a Smagorinski turbulent model have been recently proposed

G. Stabile, F. Ballarin, G. Zuccarino and G. Rozza. A reduced order variational multiscale approach for turbulent flows, submitted, 2018, https://arxiv.org/abs/1809.11101

F. Ballarin, T. Chacón Rebollo, E. Delgado Ávila, M. Gómez Mármol, and G. Rozza, *Certified Reduced Basis VMS-Smagorinsky model for natural convection flow in a cavity with variable height*. ArXiV preprint. http://arxiv.org/abs/1902.05729

T. Chacón Rebollo, E. Delgado Ávila, M. Gómez Mármol, F. Ballarin, and G. Rozza *On a certified Smagorinsky reduced basis turbulence model.* SIAM Journal on Numerical Analysis, 55 (2017) pp. 3047-3067

- Important expectations and needs dealing with industrial and cardiovascular flows.
- ROM developments in FV and also higher order methods.

Unsteady incompressible Navier-Stokes equations

- Numerical simulations on a lid driven cavity using FE discretization $\mathbb{P}_2/\mathbb{P}_2$.
- Classical stabilization technique is implemented in the high order and then projected on reduced basis.
- **RB** stabilization is based on Streamline Upwind Petrov Galerkin (SUPG) and compared with the supremizer enrichment approach
- A significant reduction in the computational cost of offline-online stabilization without supremizer could be achieved



Error comparison for Velocity (left) and Pressure (right). Parameter range in offline stage is $Re \in [100, 200]$, FE dimension $\mathcal{N}=3327$, RB dimension, N = 60 (with supremizer), N = 40 (without supremizer).

S. Ali, S. Hijazi, G. Stabile, F. Ballarin, G. Rozza, The effort of increasing Reynolds number in POD-Galerkin Reduced Order Methods: from laminar to turbulent flows, for the special volume of the FEF conference, in press, 2019.

#Fluid Dynamics #Embedded-Immersed FEMs #ROMS on a Background Geometry with Efthymios Karatzas, Francesco Ballarin, Giovanni Stabile Guglielmo Scovazzi, Leo Nouveau, Nabil Atallah



Teth_Velocity Mognitude 0.000e+00 0.49 0.98 1.47 1.965e+00 Truth_Velocity Mognitude 0.000e+00 0.49 0.98 1.47 1.955e+00







ROMS for systems with Parametric Geometry and Embedded FEMs

- Equations: Multiphase fluid dynamics, viscous steady and unsteady incompressible flows, Stokes, Navier-Stokes, Cahn-Hilliard
- Methodology: SBM, CutFEM, EBM/IBM, differences/advantages with respect to a reference domain approach



E.N. Karatzas, G. Stabile, L. Nouveau, G. Scovazzi, G. Rozza. A reduced basis approach for PDEs on parametrized geometries based on the shifted boundary finite element method and application to a Stokes flow, CMAME, (347), pp. 568-587, 2019

Some ROM challenges for Embedded FEMs

Model for multiphase fluids dynamics: hydrodynamic effects/polymer fluids





$$c_t - \frac{1}{Pe} \nabla \cdot (b(c) \nabla w) + \mathbf{u} \cdot \nabla c = 0,$$

$$w = \Phi'(c) - \gamma^2 \Delta c, \ \Phi(c) = \frac{1}{4} (1 - c^2)^2$$

 $\mathbf{u}_t - \frac{1}{Re} \Delta \mathbf{u} + \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p + Kc \nabla w = 0 ,$ $\nabla \cdot \mathbf{u} = 0, \ \mathbf{u} = \frac{1+c}{2} \mathbf{u}_1 + \frac{1-c}{2} \mathbf{u}_2$

Notation: concentration c, chemical potential w, capillary number K, interface parameter γ , mobility function $b(\cdot)$, Péclet adv/diff transport rate number Pe.

 Software packages used, Offline: Nalu, ngsxfem, Online: ITHACA, RBniCS.

#FSI

Monolithic ROMs for FSI problems with Francesco Ballarin, Monica Nonino and Yvon Maday



Formulation of FSI problems

- Fluid variables: (**u**_f, **p**, **d**_f),
- Structure variables: (**u**_s, **d**_s),
- Fluid-structure interaction problem three-fields formulation:

$$\left\{ \begin{array}{ll} F(\boldsymbol{u}_{f},\boldsymbol{p},\boldsymbol{d}_{f};\boldsymbol{d}_{s})=0, & \text{Fluid} \\ S(\boldsymbol{u}_{s},\boldsymbol{d}_{s})=0, & \text{Structure} \\ I(\boldsymbol{d}_{f},\boldsymbol{d}_{s})=0, & \text{Interface} \end{array} \right.$$

subject to interface (coupling) conditions

$$\begin{cases} \mathbf{d}_s - \mathbf{d}_f = 0 & \text{on } \Gamma, & \text{geometric continuity} \\ \mathbf{u}_s - \mathbf{u}_f = 0 & \text{on } \Gamma, & \text{velocity continuity} \\ \sigma_f \cdot n_f + \sigma_s \cdot n_s = 0 & \text{on } \Gamma, & \text{balance of normal forces.} \end{cases}$$



Reduced order monolithic formulation of FSI problems

Truth Finite Element discretization (P2-P1 Taylor-Hood)

$$\begin{array}{ll} \text{For } \boldsymbol{\mu} \in \mathcal{D}, \text{ solve} & \text{ large } \mathcal{N} \\ F^{\mathcal{N}}(\boldsymbol{u}_{f}^{\mathcal{N}}(\boldsymbol{\mu}), \boldsymbol{p}^{\mathcal{N}}(\boldsymbol{\mu}), \boldsymbol{d}_{f}^{\mathcal{N}}(\boldsymbol{\mu}); \boldsymbol{d}_{s}^{\mathcal{N}}(\boldsymbol{\mu}); \boldsymbol{\mu}) = 0 & \text{ Fluid } \\ S^{\mathcal{N}}(\boldsymbol{u}_{s}^{\mathcal{N}}(\boldsymbol{\mu}), \boldsymbol{d}_{s}^{\mathcal{N}}(\boldsymbol{\mu}); \boldsymbol{\mu}) = 0 & \text{ Structure } \\ I^{\mathcal{N}}(\boldsymbol{d}_{f}^{\mathcal{N}}(\boldsymbol{\mu}), \boldsymbol{d}_{s}^{\mathcal{N}}(\boldsymbol{\mu}); \boldsymbol{\mu}) = 0 & \text{ Interface, coupled conditions } \end{array}$$

OFFLINE – Space construction and matrices assembling

- Space construction by Proper Orthogonal Decomposition for global variables.
- Additional computations related to inf-sup stabilization procedure by means of supremizer enrichment → accurate pressure recovery for balance of normal forces. [Ballarin et al., 2015], [Rozza et al., 2012], [Rozza, Veroy, 2007].

ONLINE – Galerkin projection over the enriched space

For $\mu \in \mathcal{D}$, solve	$N\ll \mathcal{N}$
$F^{\mathbf{N}}(\boldsymbol{u}_{f}^{\mathbf{N}}(\boldsymbol{\mu}), \boldsymbol{p}^{\mathbf{N}}(\boldsymbol{\mu}), \boldsymbol{d}_{f}^{\mathbf{N}}(\boldsymbol{\mu}); \boldsymbol{d}_{s}^{\mathbf{N}}(\boldsymbol{\mu}); \boldsymbol{\mu}) = 0$ $S^{\mathbf{N}}(\boldsymbol{u}_{s}^{\mathbf{N}}(\boldsymbol{\mu}), \boldsymbol{d}_{s}^{\mathbf{N}}(\boldsymbol{\mu}); \boldsymbol{\mu}) = 0$	Reduced fluid Reduced structure
$I^{(a_{f}^{(a)}(\mu))}, a_{s}^{(a)}(\mu); \mu) = 0$	Reduced Interface, coupled conditions
Our approach:	

POD–Galerkin method for global variables u, p, d (monolithic approach), time dependent,

• capability to parametrize the initial configuration (geometry).

G. Rozza ROM for PDI

Ongoing applications to cardiovascular modelling

Increase leaflet length:

(same inlet velocity)



Increase inlet velocity:

(same leaflet length)



Ongoing applications to cardiovascular modelling



- Ballarin, Rozza. POD–Galerkin monolithic reduced order models for parametrized fluid-structure interaction problems. IJNMF, 82(12):1010–1034, 2016.
- F. Ballarin, G. Rozza, Y. Maday. Reduced-order semi-implicit schemes for fluid-structure interaction problems. MS&A, vol. 17, 2017. Springer [segregated approach]

Introduction on Reduced Order Methods in CFD: State of the art and Perspectives



Reduction of Kolmogorov n-width

- Coupled problem: tube with a fluid, and solid walls at the top and at the bottom.
- Time $t \in [0, T]$ is the only parameter; the problem is transport dominated.

Example: pressure (t = 0.0024, 0.006, 0.011)*:*



Pressure wave travelling through the domain, causing a slower decay of the Kolmogorov n-width of the solution manifold.

• Offline step (preprocessing): store the snapshots and then stretch them so that we move the peak of the pressure wave at the same point.

Example: preprocessed pressure (t = 0.0024, 0.006, 0.011):



N. Cagniart, Y. Maday, B. Stamm. Model Order Reduction for problems with large convection effects. https://hal.upmc.fr/hal-01395571. 2016.

Results: comparison of the rate of decay of the singular values of the POD on the pressure and displacement.



#Advanced #CFD & #Structural #Mechanics

ROM for Stability and Bifurcations Studies with Martin Hess, Federico Pichi Annalisa Quaini, Max Gunzburger and Anthony Patera





Bifurcation analysis with ROMs in fluid dynamics

Bifurcation and stability analysis of parametrized Navier-Stokes models by global and localized ROMs

- Stability studies in nonlinear problems are very expensive.
- Understand and detect complex phenomena, such as bifurcations, leading to loss of uniqueness with changing geometry and physical parameters, using spectral element simulations.
- Efficient reduced numerical techniques to detect steady and Hopf bifurcations and branching.
- continuation, eigenvalues analysis, long-term goal: use in multi-physics studies.



- this work is presented in
- M. Hess, A. Quaini, G. Rozza. "Reduced Basis Model Order Reduction for Navier-Stokes equations in domains with walls of varying curvature", 2019, ArXiv arxiv.org/abs/1901.03708
- M. Hess, A. Quaini, and G. Rozza, "A Spectral Element Reduced Basis Method for Navier-Stokes Equations with Geometric Variations", 2018, ArXiv arxiv.org/abs/1812.11051
- M. Hess, A. Alla, A. Quaini, G. Rozza, and M. Gunzburger, "A Localized Reduced-Order Modeling Approach for PDEs with Bifurcating Solutions", 2018, ArXiv arxiv.org/abs/1807.08851

Some ROM challenges in CFD

 Complex CFD problems in 3D setting characterized by bifurcations, e.g. Coanda effect during mitral valves regurgitation, influence of more complex geometries and multiphysics on bifurcations and stability.



Investigations on bifurcations and loss of uniqueness of the solution require ROM for parametrized eigenvalue analysis. [Pitton, Rozza, 2017, Journal of Scientific Computing; Pitton, Quaini, Rozza, 2017, Journal of Computational physics]



Some ROM challenges in Structural Mechanics

 Computational mechanics problems to study the deformation of a plate under compression (load λ and shape ψ) and the bifurcations of the Von Kaímań model through the linearized eigenproblem.

[Pichi, F. , Rozza, G., 2018, Reduced basis approaches for parametrized bifurcation problems held by non-linear Von Kármán equations, arXiv:1804.02014]



Secondary bifurcations, better computations of parametric stability factors

 Quantum mechanics problems to study the Gross–Pitaevskii equation that describes the ground state of a quantum system of identical bosons.
 [Pichi, F., Quaini, A., Rozza, G., 2019, Reduced deflation technique in bifurcating phenomena: application to the Gross–Pitaevskii equation, In progress]

Further investigations on: Empirical Interpolation techniques, Neo-Hookean beam 2D/3D problem and a posteriori error estimate are in progress. FVG - MIT project ROM2S

#UQ #CFD # FEM Weighted reduced methods for parametrized problems with random inputs with Francesco Ballarin, Davide Torlo and Luca Venturi





Uncertainty quantification problems with weighted reduced approach

- extension of (deterministic) reduced order methods to stochastic PDEs:
 - weighting to account for the probability space;
 - sampling from representative probability distribution;
 - exploitation of sparse grids to reduce the computational cost for high dimensional parameter spaces to break the curse of dimensionality;
- application to advection dominated problems by means of reduced order stabilization techniques.



L. Venturi, D. Torlo, F. Ballarin, and G. Rozza. "Weighted reduced order methods for parametrized partial differential equations with random inputs". Uncertainty Modeling for Engineering Applications, Springer, 2019.

L. Venturi, F. Ballarin, and G. Rozza. "A weighted POD method for elliptic PDEs with random inputs". Journal of Scientific Computing, in press, 2019.

D. Torlo, F. Ballarin, and G. Rozza. "Stabilized weighted reduced basis methods for parametrized advection dominated problems with random inputs". SIAM/ASA Journal on Uncertainty Quantification, 2018.

Former works in collaboration with A. Quarteroni and C. Peng

G. Rozza ROM for PDEs

#Applications # ROMs # CFD # OFCPs # CAD # CABGs

Parametrized reduced order optimal control for blood flows in patients' specific geometries with Zakia Zainib, Francesco Ballarin Piero Triverio, Laura Jiménez, Stephen Fremes



Mysteries of the heart: U of T Engineering professor developing solutions for coronary artery disease with mathematical models



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Triple Coronary Artery Bypass Grafts (CABGs)

- Medical image data (CT-scan) from Sunnybrook Health Sciences Center, Toronto, Canada.
- Three grafts attached to three different diseased arteries,
 - Right internal mammary artery (RIMA) to left anterior descending artery (LAD).





Vein graft

- Vein graft to posterior descending artery (PDA).

Vein graft

PDA

OM1



F. Auricchio, M. Conti, A. Lefieux, S. Morganti, A. Reali, G. Rozza, and A. Veneziani. Cardiovascular Mechanics, chapter: Computational Methods in Cardiovascular Mechanics. CRC Press Taylor and Francis Group, 2018.
Problem description:

Navier-Stokes equations constrained boundary control with physical parametrization, and geometrical and physiological data assimilation.

$$\begin{split} \min_{(\mathbf{v}, u)} \mathcal{J}\left(\mathbf{v}\left(\mu\right), p\left(\mu\right), u\left(\mu\right)\right) &= \frac{1}{2} \int_{\Omega} |\mathbf{v}\left(\mu\right) - \mathbf{v}_{d}|^{2} + \frac{\alpha}{2} \int_{\Gamma_{out}} |u\left(\mu\right)|^{2} \\ \text{subject to} & \begin{cases} -\eta \Delta \mathbf{v}\left(\mu\right) + \left(\mathbf{v}\left(\mu\right) \cdot \nabla\right) \mathbf{v}\left(\mu\right) + \nabla p\left(\mu\right) = \mathbf{0}, & \text{in } \Omega \\ \nabla \cdot \mathbf{v}\left(\mu\right) = \mathbf{0}, & \text{in } \Omega \\ \mathbf{v}\left(\mu\right) = \mathbf{v}_{in}, & \text{on } \Gamma_{in} \\ \mathbf{v}\left(\mu\right) = \mathbf{0}, & \text{on } \Gamma_{wall} \\ \eta \nabla \mathbf{v}\left(\mu\right) \cdot \mathbf{n} - p\left(\mu\right) \mathbf{n} = u\left(\mu\right) & \text{on } \Gamma_{out} \end{split}$$

- Patient-specific computational domain Ω.
- Patient-specific physiological data v_d acquired through 4D-MRI.

The goal: rely on simplier Neumann boundary conditions, but tune $u(\mu)$ to best match v_d acquired by measurement of the velocity profile.



Figure: Reduced order optimal control pipeline: an overview

Negri, Manzoni, and Rozza, Comp. Math. App., 2015. Negri, Rozza, Manzoni, and Quarteroni, SIAM J. Sci. Comp., 2013. G. Rozza ROM for PDEs

Reliability of the reduced order model

Test case: Vein graft to OM1, $\mu = \mathsf{Re} \in [45, 50]$





Figure: Velocity magnitude

Figure: Control magnitude



Figure: Relative error b/w FE and POD approximations of variables

	FE approx.	ROM approx.
Mesh size	27398	-
Degrees of freedom	280274	43
CPU time (secs)	634	118 (online)







Figure: Relative error b/w FE and POD reduction in $\ensuremath{\mathcal{J}}$

#Applications #Environmental #CFD #DataAssimilation #InverseProblems

Reduced Order Methods for Parametrized Optimal Flow Control in Environmental Marine Sciences with Maria Strazzullo and Francesco Ballarin



Pollutant Control on Gulf of Trieste, Italy

Motivations: forecasting, data assimilation, ecological and touristic and geographical interest. **Collaborations:** National Institute of Oceanography and Applied Geophysics, OGS, Trieste, Italy. **Problem formulation** $y \in H_{\Gamma_{\infty}}^{1}(\Omega), u \in \mathbb{R}, y_{d} \in \mathbb{R}$ (safeguard threshold)

Weak formulation

Minimise with respect to $(y(\boldsymbol{\mu}), u(\boldsymbol{\mu})) \in Y \times U$

$$\frac{1}{2}\int_{\Omega_{OBS}}(y(\boldsymbol{\mu})-y_d)^2 \ d\Omega_y + \frac{\alpha}{2}\int_{\Omega_u}u(\boldsymbol{\mu})^2 \ d\Omega_u$$

constrained to an advection-diffusion state equation:

$$a(y(\mu),q)=c(u(\mu),q), \quad \forall q\in Q.$$

Boundaries:

 Γ_D = coasts, Γ_N = Adriatic Sea. **Subdomains**: Ω_{OBS} = Natural area of Miramare;

 Ω_u = Source of pollutant (in front of the city of Trieste).









Weak Formulation of the Parametric Inverse problem

•
$$a: Y \times Q \to \mathbb{R}:$$

 $a(y, q, \mu) = \int_{\Omega} (\nu(\mu) \nabla y \cdot \nabla q + \beta(\mu) \cdot \nabla yq) \ d\Omega,$

• $c: U \times Q \to \mathbb{R}$: $c(u,q) = Lu \int_{\Omega_u} q d\Omega_u, \quad [L = 10^3 \to \text{ non-dimensional system}]$

Parameters $(\mathcal{D} = [0.5, 1] imes [-1, 1] imes [-1, 1])$

 $u(\boldsymbol{\mu}) \equiv \mu_1 \text{ is the diffusivity parameter,}$

 $oldsymbol{eta}(oldsymbol{\mu}) = [eta_1(\mu_2),eta_2(\mu_3)]$ is the transport field,

Control and cost functional value for several parameters

 $\begin{array}{cccc} \mu & u & J_r \\ \text{No wind} & (1,0,0) & 7.6901 \cdot 10^{-1} & 5.1320 \cdot 10^{-5} \\ \text{Bora} & (1,-1,1) & 7.3698 \cdot 10^{-1} & 4.9167 \cdot 10^{-5} \\ \text{Scirocco} & (1,1,-1) & 8.0800 \cdot 10^{-1} & 5.3417 \cdot 10^{-5} \end{array}$

Time of a run: $t_N = 2.79s$, $t_N = 2.41 \cdot 10^{-2}s$. Dimensions: N = 5639 and N = 20.

Uncontrolled Solution 5.464e-09 0.25 0.5 0.75 1.000e+00



RB Solution -4.266e-09 0.25 0.5 0.75 1.000e+00

[Strazzullo et al., Model Reduction for Parametrized Optimal Control Problems in Environmental Marine Sciences and Engineering, SIAM SISC, 40:4, B1055-B1079, 2018]

Numerical Results: FE - POD Errors



Bora Errors. Bottom left: monolithic (one POD for $U(\mu) = (y(\mu), u(\mu), q(\mu))$) and partitioned (different POD reductions for state, control and adjoint variables) error comparison.

[Strazzullo et al., Model Reduction for Parametrized Optimal Control Problems in Environmental Marine Sciences and Engineering. SIAM SISC, 40:4, B1055-B1079, 2018]

Application: Oceanographic Solution Tracking

Motivations: unify *standard model* and *data* giving more reliable simulations *as quickly as possible*.

Aim: make the $y \in H_0^1(\Omega)$ the most similar to a given data y_d (Gulf Stream Dynamic).

$OFCP(\mu)$ governed by Quasi-Geostrophic Equation

given $\mu \in [10^{-4}, 1] \times [10^{-4}, 1] \times [10^{-4}, 0.045^2]$, find $(y(\mu), u(\mu)) \in Y \times U := L^2(\Omega)$ which solves

$$\begin{split} \min_{(y,u)} \frac{1}{2} \int_{\Omega} (y(\boldsymbol{\mu}) - y_d)^2 \ d\Omega + \frac{\alpha}{2} \int_{\Omega} u(\boldsymbol{\mu})^2 \ d\Omega \\ \text{s.t.} \begin{cases} \frac{\partial y}{\partial x_0} + \mu_1 \Delta y + \mu_2 \Delta^2 y + \mu_3 \left(\frac{\partial y}{\partial x_0} \frac{\partial \Delta y}{\partial x_1} - \frac{\partial \Delta y}{\partial x_0} \frac{\partial y}{\partial x_1} \right) = u & \text{in } \Omega \\ y = 0, & \text{on } \partial\Omega, \\ \Delta y = 0, & \text{on } \partial\Omega. \end{cases} \end{split}$$



Streamline Formulation:

y = streamfunction, $\Delta y = -$ vorticity. The velocity field \mathbf{v} of Oceanic current, solution of the Geophysical Navier-Stokes Equation [Navier-Stokes Equation + Earth rotation effect], could be recovered by $(v_1, v_2) = (y_{x_1}, -y_{x_0})$.

Results: Oceanographic Solution Tracking





Desired Solution 0.000e+00 0.36 0.537.108e-01



FE Solution -3.458e-03 0.35 0.537.100e-01



[Strazzullo *et al.*, Model Reduction for Parametrized Optimal Control Problems in Environmental Marine Sciences and Engineering. SIAM SISC, 40:4, B1055-B1079, 2018]

G. Rozza ROMs for $OFCP(\mu)$

Speed up and system dimensions
$$\boldsymbol{\mu} = (10^{-4}, 0.07^3, 0.045^2)$$

Time of a run: $t_N = 5.59s$, $t_N = 2.38 \cdot 10^{-1}s$. Dimensions: N = 6490 and N = 125.

 $\begin{array}{l} \mu_1, \mu_2: \text{ diffusivity parameter,} \\ \mu_3: \text{ advection parameter,} \\ N_{\max}: 100, \\ \alpha: 10^{-5}. \end{array}$

Numerical Results: State Equation Stokes

Aim: recover $\mathbf{v}_d = [\mu_3(8(v^3 - v^2 - v + 1) + 2(-v^3 - v^2 + v + 1)), 0]$ in Ω_{OBS} with a Neumann control.

$\mathsf{OFCP}(\mu)$ governed by time dependent Stokes

given $\mu \in [1/20, 1/6] \times [1, 2] \times [1, 3]$, find $(\nu(\mu), p(\mu), u(\mu)) \in \mathcal{X}$ which solves

$$\begin{split} \min_{(\mathbf{v},p,\mathbf{u})\in X} \frac{1}{2} \int_0^T \int_{\Gamma_{OBS}} (\mathbf{v} - \mathbf{v}_d(\mu_3))^2 ds dt + \frac{\alpha_1}{2} \int_0^T \int_{\Gamma_C} \mathbf{u}^2 ds dt + \frac{\alpha_2}{2} \int_0^T \int_{\Gamma_C} |\nabla \mathbf{u} \cdot \mathbf{t}|^2 ds dt \\ s.t. \begin{cases} \mathbf{v}_t - \mu_1 \Delta \mathbf{v} + \nabla p = 0 & \text{in } \Omega(\mu_2) \times [0, 1], \\ \text{div}(\mathbf{v}) = 0 & \text{in } \Omega(\mu_2) \times [0, 1], \\ \mathbf{v} = \mathbf{g} & \text{on } \Gamma_{IN}(\mu_2) \times [0, 1], \\ \mathbf{v} = 0 & \text{on } \Gamma_D(\mu_2) \times [0, 1], \\ -p\mathbf{n} + \nabla \mathbf{v} \cdot \mathbf{n} = \mathbf{u} & \text{on } \Gamma_C(\mu_2) \times [0, 1], \\ \mathbf{v}(0) = \mathbf{v}_0 & \text{in } \Omega(\mu_2) \times \{0\}. \end{split}$$



 $μ_1$: diffusivity parameter, $μ_2$: length of $Ω_2$, N_{max} : 70, N_t : 20, $α_1, α_2$: 10⁻³, 10⁻⁴.

Numerical Results: State Equation Stokes - results



[Strazzullo, Zainib, Ballarin, Rozza, Reduced order methods for parametrized nonlinear and time dependent optimal flow control problems, towards applications in biomedical and environmental sciences. *In preparation*]

#CFD #FV

ROM for Finite Volume Discretization of viscous flows with stable pressure with Giovanni Stabile, Saddam Hijazi, Andrea Lario and Matteo Zancanaro





Why Finite Volumes?

It became the standard for real world applications in several engineering fields (Aeronautics, Industrial flows, Automotive, Naval Engineering)

For increasing Reynolds numbers there are less problems concerning stability and several **turbulence models** are already available.

The lid driven cavity problem

The first proposed benchmark consists into the well known lid driven cavity problem:



The mesh is structured and counts 40000 quadrilateral cells, 200 on each dimension of the square. The kinematic viscosity is equal to $\nu = 1 \times 10^{-4} \text{m}^2/\text{s}$ that leads to a Reynolds number of 10000. In this case no parametrization is introduced.

Comparison of the velocity and pressure fields for high fidelity, SUP-ROM and PPE-ROM.

The fields are depicted for different time instant equal to t = 0.2s, 0.5s, 1s and 5s.





The table contains the cumulative eigenvalues for the lid driven cavity test. The last column contains the value of the inf-sup constant, in the supremizer stabilization case, for different different number of supremizer modes and with a fixed number of velocity and pressure modes.

N Modes	u	р	S	β
1	0.978946	0.975406	0.980260	9.264e-05
2	0.994184	0.991528	0.995232	9.264e-05
3	0.997737	0.995385	0.997912	7.175e-04
4	0.998990	0.998116	0.999400	7.175e-04
5	0.999483	0.999270	0.999844	7.175e-04
10	0.999971	0.999971	0.999997	1.551e-02

The flow around a circular cylinder



The properties of the presented algorithms have been tested also with the benchmark of the **laminar flow around a circular cylinder**. In this case the viscosity have been parametrized and results refer to a parameter non experimented in the full order simulations. The parameter space is given by **5 different** values of the viscosity: $\nu \in [0.005, 0.01]$. These values of viscosity result into the values of the Reynolds number Re $\in [100, 200]$.

First four modes for velocity pressure and supremizers



Cumulative eigenvalues

N Modes	u	р	s	β
1	0.390813	0.793239	0.921046	2.608e-04
2	0.598176	0.85809	0.941746	4.492e-04
3	0.802176	0.911636	0.961438	7.869e-03
4	0.879096	0.934997	0.978072	1.662e-02
5	0.949519	0.955578	0.98669	1.662e-02
10	0.986025	0.992347	0.998307	1.098e-01
15	0.995922	0.997994	0.999732	1.199e-01

Comparison of the velocity field



UHF t=195s 0.0e+00 0.75 1.5e+00



USUP t=195s 0.0e+00 0.75 1.5e+00



UPPE t=195s 0.0e+00 0.75 1.5e+00



UHF 1=200s 0.0e+00 0.75 1.5e+00



USUP 1=200s 0.0e+00 0.75 1.5e+00

UPPE t=200s

0.0e+00 0.75 1.5e+00



UHF t=230s 0.0e+00 0.75 1.5e+00



USUP 1=230s 0.0e+00 0.75 1.5e+00



UPPE 1=230s 0.0e+00 0.75 1.5e+00



UHF t=270s 0.0e+00 0.75 1.5e+00



USUP t=270s 0.0e+00 0.75 1.5e+00



UPPE t=270s 0.0e+00 0.75 1.5e+00

Comparison of the pressure field



G. Rozza ROM for PDEs

Comparison on the same time window ans computational costs



- The velocity field is reproduced in a more accurate way using the Poisson equation approach. This is due to the "pollution" given by the non-necessary supremizer modes.
- On the other side the **pressure** field is better reproduced using a supremizer approach.
- The cavity example has run serially with OpenFOAM 5.0 (i7 laptop).
- The cylinder example has run in parallel with OpenFOAM 5.0.
- The reduced order models have run in serial in ITHACA-FV. It is available on github https://github.com/mathLab/ITHACA-FV.
- In the worst case the speed up is equal to approx. 200.



G. Stabile and G. Rozza, Stabilized Reduced order POD-Galerkin techniques for finite volume approximation of the parametrized Navier–Stokes equations, Computer & Fluids, 2018.

S. Ali, S. Hijazi, G. Stabile, F. Ballarin, G. Rozza, The effort of increasing Reynolds number in POD-Galerkin Reduced Order Methods: from laminar to turbulent flows, FEF, 2017, in press, 2019.

#CFD

ROM and Finite Volume Discretization for fluid mechanics of turbulent flows Joint Work with G. Stabile, S. Hijazi, S. Georgaka, K. Star, M. Zancanaro

Why Finite Volumes?

The finite element method is nowadays the standard in the reduced order modelling community so why to use a different discretisation technique?



It became the standard for **real world applications** in several engineering fields (Aeronautics, Industrial flows, Automotive, Naval Engineering)



One can find well developed open source libraries, **OpenFOAM** is today probably the most spread CFD open-source solver.



For increasing Reynolds numbers there are less problems concerning stability and several **turbulence models** are already available.



More difficulties into the affine decomposition of the differential operators.



The ROM methodology, mainly developed for **FEM solvers**, needs to be adapted.

The **geometrical parametrization** includes many **more difficulties** with respect to a finite element setting

Reduced order methods for FV - Laminar Flows

Issues in FV and Reduced Order Modelling

To export the ROM methodology, mainly developed for finite element solvers, into a **Finite Volume setting** several issues need to be tackled.

- Adapt ROMs to finite volume approximations [Haasdonk and Ohlberger (2008)].
- Geometrical Parametrisation [Drohmann et al (2009)].
- **Stabilisation** issues for **incompressible** flows [Rozza et al., Noack, Akhtar, Iliescu, Iollo, ..]
- Stabilisation for compressible flows and long time intervals [Carlberg et al (2017), Balajewicz et al (2016), Fick et al 2017)][Carlberg 2018].
- Develop ROMs beyond the laminar assumption [Lorenzi 2016].

Sta-Ro (2018). Finite volume POD-Galerkin stabilized reduced order methods for the parametrised incompressible Navier-Stokes equations. *Computers & Fluids*, 173, 273-284.

Sta-Hi-Mo-Lo-Ro (2017) POD-Galerkin reduced order methods for CFD using finite volume discretisation: vortex shedding around a circular cylinder. Communications in Applied and Industrial Mathematics, 8 (1), pp 210-236, 2017

Reduced order methods for finite volume discretization

Reduced order methods for turbulent flows

- The goal is to develop reduced order methods dedicated for the treatment of turbulent flows.
- Development of Reduced Order Models which merge projection-based methods and data-driven techniques.
- The model has been tested on benchmark cases like the Pitz-Daily case and the flow around a circular cylinder.
- The **Reynolds** number in the cases is up to $Re = 10^4 10^6$.







The Idea

RANS Equations.

• The $k - \omega$ turbulence model, has been used in this work

$$\begin{cases} \frac{\partial u}{\partial t} + \nabla \cdot (\boldsymbol{u} \otimes \boldsymbol{u}) = \text{lam. terms} + g(\nu_t), & \text{in } \Omega \times [0, T], \\ \nabla \cdot \boldsymbol{u} = 0, & \text{in } \Omega \times [0, T], \\ \boldsymbol{u}(t, \boldsymbol{x}) = \boldsymbol{f}(\boldsymbol{x}, \boldsymbol{\mu}), & \text{on } \Gamma_{ln} \times [0, T], \\ \boldsymbol{u}(t, \boldsymbol{x}) = \boldsymbol{0}, & \text{on } \Gamma_0 \times [0, T], \\ (\nu \nabla \boldsymbol{u} - \boldsymbol{p} \boldsymbol{l}) \boldsymbol{n} = \boldsymbol{0}, & \text{on } \Gamma_{Out} \times [0, T], \\ (\boldsymbol{u}(0, \boldsymbol{x}) = \boldsymbol{k}(\boldsymbol{x}), & \text{in } (\Omega, 0), \\ \nu_t = F(k, \omega), & \text{in } \Omega, \\ \text{Transport-Diffusion equation for } k, \\ \text{Transport-Diffusion equation for } \omega, \end{cases}$$

k is the turbulent kinetic energy ω is the rate of dissipation for turbulent kinetic energy

• One could project the standard Navier Stokes equations without the eddy viscosity contribution on the modes computed using a stabilized FOM but this approach fails. \rightarrow We have to consider the contribution given by the additional eddy viscosity term.

The Reduced Order Model

 One idea could be to decompose all turbulence variables as was done with velocity and pressure and then projecting the additional PDEs onto the spaces spanned by the POD modes of the turbulence variables, namely:

$$k(\mathbf{x}, t; \boldsymbol{\mu}) \approx \sum_{i=1}^{N_k} e_i(t, \boldsymbol{\mu}) \beta_i(\mathbf{x}), \qquad (7)$$

$$\omega(\mathbf{x}, t; \boldsymbol{\mu}) \approx \sum_{i=1}^{N_{\omega}} f_i(t, \boldsymbol{\mu}) \gamma_i(\mathbf{x}), \qquad (8)$$

$$\begin{aligned} &(\beta_i, A1(k))_{L^2(\Omega)} = 0, \\ &(\gamma_i, A2(\omega))_{L^2(\Omega)} = 0, \end{aligned}$$

where A1(k) and $A2(\omega)$ are the differential operators that correspond to the transport diffusion PDEs.

- This approach is problem dependent and thus a different ROM has to be developed for each turbulence model.
- The operators *A*1(*k*) and *A*2(*ω*) have strong non-linearities and treating them in ROM is quite challenging.
- This makes the approach inconvenient, the interest is in building ROM which is more general and less expensive.

The Reduced Order Model

• We use just the decomposition of the eddy viscosity field:

$$u_t(\mathbf{x}, t; \boldsymbol{\mu}) \approx \sum_{i=1}^{N_{\nu_t}} g_i(t, \boldsymbol{\mu}) \eta_i(\mathbf{x}),$$

• The projection of the momentum equation gives:

$$\begin{cases} \boldsymbol{M}\dot{\boldsymbol{a}} = \nu(\boldsymbol{B} + \boldsymbol{B}_{T})\boldsymbol{a} - \boldsymbol{a}^{T}\boldsymbol{C}\boldsymbol{a} + \boldsymbol{g}^{T}(\boldsymbol{C}_{T1} + \boldsymbol{C}_{T2})\boldsymbol{a} - \boldsymbol{H}\boldsymbol{b}, \\ \boldsymbol{P}\boldsymbol{a} = \boldsymbol{0}, \end{cases}$$

where g is the vector of the coefficients $[g_i(t,\mu)]_{i=1}^{N_{\nu_t}}$, and the new terms are computed as follows:

$$\begin{split} B_{T_{ij}} &= \left(\phi_i, \boldsymbol{\nabla} \cdot (\boldsymbol{\nabla} \phi_j^T)\right)_{L^2(\Omega)}, \\ C_{T_{1jjk}} &= \left(\phi_i, \eta_j \Delta \phi_k\right)_{L^2(\Omega)}, \\ C_{T_{2ijk}} &= \left(\phi_i, \boldsymbol{\nabla} \cdot \eta_j (\boldsymbol{\nabla} \phi_k^T)\right)_{L^2(\Omega)} \end{split}$$

• Once the vector \boldsymbol{g} is computed, the system can be solved for \boldsymbol{a} and \boldsymbol{b} .

The Reduced Order Model

- The problem is now to compute the coefficients g of the eddy viscosity equations without relying on the projection of the equations → POD-I.
- The proper orthogonal decomposition with interpolation is a method to approximate the numerical solution of a parametric partial differential equations as combination of few solutions computed for some properly chosen parameters.

$$orall oldsymbol{\mu}_k \in \mathcal{P}_{train}, \quad oldsymbol{u}(\mu_k) pprox oldsymbol{u}^N(oldsymbol{\mu}_k) = \sum_{i=1}^N oldsymbol{s}_i(oldsymbol{\mu}_k) \phi_i,$$

$$oldsymbol{u}_{NEW}^{N} = \sum_{i=1}^{N} oldsymbol{a}_{i}(oldsymbol{\mu}_{NEW}) \phi_{i}.$$

- Each function a_i(μ) is approximated using approximated interpolant functions.
- It relies only on the snapshots: it does not require any information about the system (non-intrusive approach).
- The interpolation is carried out using Radial Basis Functions.

Numerical results : steady case

Steady state case: the backstep



Figure: The computational domain used in the numerical simulations, L is equal to 50.8 meters.

The parameter vector is $\boldsymbol{\mu} = [\mu_1, \mu_2]$

 μ_1 : the magnitude of the velocity at the inlet μ_2 : the inclination of the velocity with respect to the inlet which is measured in degrees.

Numerical results : Pitz-Daily benchmark steady case

Velocity results

- Fixed viscosity value $\nu = 10^{-3}$
- Parametrized inlet velocity in inclination and magnitude $\mu_1 \in [0.18, 0.3]$ and $\mu_2 \in [0, 30]$, Reynolds number ranges from 9.144 × 10³-1.524 × 10⁴



Figure: Velocity fields for $\mu^* = (0.22089, 24.484)$: (a) shows the DD-ROM Velocity, while in (b) one can see the ROM Velocity (without viscosity incorporated in ROM), and finally in (c) we have the FOM Velocity.

Hi-Ali-Sta-Ba-Ro (2018) The Effort of Increasing Reynolds Number in Projection-Based Reduced Order Methods: from Laminar to Turbulent Flows, *FEF Special Volume*

Pressure results

• The relative L^2 error are 2.957% and 222.96% for DD-ROM and ROM, respectively.



Figure: Pressure fields for $\mu^* = (0.22089, 24.484)$: (a) shows the DD-ROM Pressure, while in (b) one can see the ROM Pressure (without viscosity incorporated in ROM), and finally in (c) we have the FOM Pressure.

Numerical results : Flow around a cylinder, unsteady case

 Results for the mixed Data-Driven and projection-based Reduced Order Model (DD-ROM) proved accuracy and efficiency compared to the ones obtained from a fully projection-based strategy.



Figure: FOM,ROM and DD-ROM lift coefficients for the forces acting on the cylinder, in this case $Re = 10^4$. Turbulence model: K-omega.

DD-ROM relative error is in the range of 1 - 5 %, while ROM has a relative error of 20%, T_{CPUFOM} = 525.32 s, T_{CPUDD-ROM} = 1.095 s, Speed up of 479.

S. Hijazi, G. Stabile, A. Mola and G. Rozza (2018) Data-Driven POD–Galerkin reduced order model for turbulent flows POD–Galerkin reduced order model for turbulent flows, *In Preparation*

G. Rozza ROM for PDEs

#Shape parametrisation #Active Subspaces #POD-Galerkin Combined parameter and model reduction

with Marco Tezzele and Francesco Ballarin





Tezzele et al. "Combined parameter and model reduction of cardiovascular problems by means of active subspaces and POD-Galerkin methods". 2018 Tezzele et al. "Dimension reduction in heterogeneous parametric spaces with application to naval engineering shape design problems". 2018

Active subspaces property

(

In many cases the dimension of the parametrised problem is only artificially high

Active subspaces property identifies a set of important directions in the space of all inputs

$$f : \mathbb{R}^m \to \mathbb{R} \qquad \mathbf{x} \in \mathbb{R}^m$$
$$\mathbf{C} = \mathbb{E}\left[\nabla_{\mathbf{x}} f \, \nabla_{\mathbf{x}} f^T\right] = \int (\nabla_{\mathbf{x}} f) (\nabla_{\mathbf{x}} f)^T \rho \, d\mathbf{x}$$
$$\mathbf{C} = \mathbf{W} \mathbf{A} \mathbf{W}^T$$

f is a scalar function that takes as arguments the parameters \boldsymbol{x}

C is the uncentered covariance matrix of the gradients of f, symmetric, positive semidefinite

E is the expected value and rho a probability density function

We define the active subspace to be the range of the first n eigenvectors of W

$$\mathbf{W} = [\mathbf{W_1} \quad \mathbf{W_2}] \in \mathbb{M}^{m imes m} \qquad \mathbf{\Lambda} = \begin{bmatrix} \mathbf{\Lambda_1} & \\ & \mathbf{\Lambda_2} \end{bmatrix}$$

With the basis identified, we can map forward to the active subspace. So y is the active variable and z the inactive one. The surrogate model g is used to approximate f

$$\mathbf{y} = \mathbf{W_1^T} \mathbf{x} \in \mathbb{R}^n \qquad \mathbf{z} = \mathbf{W_2^T} \mathbf{x} \in \mathbb{R}^{m-n} \qquad f(\mathbf{x}) \approx g(\mathbf{W_1^T} \mathbf{x}) = g(\mathbf{y})$$

Constantine. "Active subspaces: Emerging ideas for dimension reduction in parameter studies." SIAM, 2015.

Active Subspaces - A quadratic example



M. Tezzele, F. Ballarin and G. Rozza "Combined parameter and model reduction of cardiovascular problems by means of active subspaces and POD-Galerkin methods". 2018
M. Tezzele, F. Salmoiraghi, A. Mola, G. Rozza. "Dimension reduction in heterogeneous parametric spaces with application to naval engineering shape design problems". 2018

Flow across parametrised carotid bifurcations

- Vessels geometry strongly influences hemodynamics behaviour.
- The output function is the relative pressure drop of the two branches, computing the integral of the pressure on selected sections.



We deform the carotid after the bifurcation moving 10 RBF control points (in red) solving an interpolation system.





Deformed carotid with the deforming control points (red) and the undeformed state (black)

Spectral analysis

- The two dimensional active subspace spanned by the first two eigenvectors of the covariance matrix seems to better capture the behaviour of the output function. We use this information perform a further reduction by a **POD-Galerkin ROM**.
- We exploit a 2-dimensional active subspace to compute the POD snapshots in a reduced space with respect to the full 10-dimensional parameter space.
- Typical reduced space dimensions and computational speedup for cardiovascular flows: 500:1.



POD analysis

Here the POD singular values for velocity, supremizers and pressure, as a function of the number N of selected POD modes:





Pressure

- The standard approach presents a slower decay, meaning that it has to deal with a considerably larger solution manifold.
- The combined methodology is able to reach relative errors which are up to one order of magnitude smaller when compared to the standard one, for both velocity and pressure when N = 20.


#GeometricalMorphing #Industrial #applications #FFD A full data-driven computational pipeline with Marco Tezzele, Nicola Demo, Andrea Mola





PyGeM: Python Geometrical Morphing

PyGeM is a python library using Free Form Deformation, Radial Basis Function and Inverse Distance Weighting interpolation technique to parametrize and morph complex geometries. It is developed by N. Demo and M. Tezzele [*]



The main focus of PyGeM is to interact with the major industrial file formats used for CAD management. Since it has to integrate itself in the industrial workflow we have chosen python

Morphing of the bumper using an OpenFOAM file. DrivAer model.



[*] PyGeM on Github: github.com/mathLab/PyGeM

- It allows to handle:
 - Computer Aided Design files (.iges, .step and .stl)
 - Mesh files (.unv and OpenFOAM)
 - Output files (.vtk)

Tool for the automatic shape parametrization

- 1. Mapping the physical domain to the reference one: ψ
- 2. Moving some control points to deform the lattice: \hat{T}
- 3. Mapping back to the physical domain: ψ^{-1}
- FFD: composition of the three maps









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Efficient and accurate geometrical parametrization techniques

- At the state of the art free-form parametrization techniques for geometries are receiving a growing interest, in view of strong integration with CAD tools, as well as for design and shape optimization
- Extending isogeometric analysis (IGA) for viscous flows in the reduced basis context (AMSES, 2016, Salmoiraghi et al., QUIET 2017 special issue, Garotta et al.)

$$T(\underline{x},\mu):\Omega\to\Omega_0(\mu)$$



In collaboration with: F. Salmoiraghi, N. Demo, M. Tezzele, F. Ballarin, L. Heltai, A. Mola (SISSA), H. Telib (Optimad-PoliTo), F. Garotta

Hull optimization pipeline - From FFD to PODI



- Given the time-average solutions, we combine the vectors containing the average force coefficients with the proper orthogonal decomposition (POD) interpolation technique implemented in EZyRB.
- Here we have the first POD modes and the optimized bulb.









Reduced Order Model for industrial shape problems



In collaboration with Fincantieri, leader in cruise ship manifacturing, we developed an innovative pipeline involving **data-driven** reduced order modeling techniques for shape optimization in naval problems.

- Shape parametrization (FFD)
- Proper orthogonal decomposition with interpolation



• Dynamic mode decomposition





Reduced Order Model for industrial shape problems

- POR FESR: SOPHYA the main goal of the project is to improve planing yacht hulls the performance in non-calm sea conditions. A set of specific methodologies have been developed to be able to parameterize the hull geometry and carry out a shape optimization campaign based both on high fidelity RANS and non-intrusive ROM simulations.
- POR FESR: PRELICA the main goal of the project is to improve ship propeller performance both in terms of thrust and acoustic emissions. A specific python package (BladeX) has been developed to generate parametrized propeller geometries. The optimal propeller shape has been identified making use of both high order LES and non-intrusive ROM hydroacoustic simulations.





Vision and Perspective: to real-time computing

Model order reduction for web server: from biomedical to naval applications



CSE-Apps

- HPC, data science
- Web computing
- Digital twin
- 3D printing
- SMACT Industry4.0



Conclusion

- It is time to better integrate Data, Modelling, Analysis, Numerics, Control, Optimization and Uncertainty Quantification in a new parametrized, reduced and coupled paradigm.
- We need to draw the attention to the fact that "Science and Industry advance with Mathematics".
- Applied Mathematics as propeller for Innovation and Technology Transfer by a new generation of computational scientists.



Thanks for your attention!

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- MIUR-PRIN project "Mathematical and numerical modelling of the cardiovascular system, and their clinical applications", 2014-2016
- INDAM-GNCS 2015, "Computational Reduction Strategies for CFD and Fluid-Structure Interaction Problems"
- INDAM-GNCS 2016-2017 "Numerical methods for model order reduction of PDEs"
- COST, European Union Cooperation in Science and Technology, TD 1307 EU-MORNET Action (http://www.eu-mor.net)
- PAR-FSC 2014-2020, Regione Friuli Venezia Giulia, UBE
- POR-FESR, 2014-2020, Regione Friuli Venezia Giulia, SOPHYA, PRELICA, UBE 2
- TRIM, INSEAN-CNR, 2016
- HPC resources: CINECA, INFN, SISSA-ICTP
- MIUR FARE-X-AROMA-CFD project
- MIT projects: "Probabilistic Multi-disciplinary Ship Design using Reduced Order Methods and Machine Learning Tools", "ROM2S Reduced Order Methods at MIT and SISSA".

Thanks for your attention!