Warming Stripes, Ed Hawkings, Climate Lab Book







On the modeling of wrinkling instabilities using isogeometric shell analysis

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Outline

1 Introduction

Wrinkling Basics

- **3** Isogeometric Shell Analysis
- **4** Path-Following Methods

5 Results

6 Conclusions and Future Work



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Introduction - Aim

Develop a robust and efficient strategy for the modelling of wrinkles using isogeometric analysis

Introduction - Aim





Introduction - Aim



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Wrinkling Basics - Energy Balance

Foundation vs Bending



Tension vs Bending



Wrinkling in a tensioned sheet ²

Folding in a floating sheet ¹

¹L. Pocivavsek et al. (2008). "Stress and fold localization in thin elastic membranes". In: Science. ISSN: 00368075. DOI: 10.1126/science.1154069

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Wrinkling Basics - Energy Balance



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Wrinkling Basics - Buckling Instabilities



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³W. Wong et al. (2006). "Wrinkled membranes I: experiments". In: Journal of Mechanics of Materials and Structures 1.1, pp. 3–25. ISSN: 1559-3959. DOI: 10.2140/jomms.2006.1.3

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Wrinkling Basics - Buckling Instabilities



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Buckling/Wrinkling of a sheared sheet³

³W. Wong et al. (2006). "Wrinkled membranes I: experiments". In: Journal of Mechanics of Materials and Structures 1.1, pp. 3–25. ISSN: 1559-3959. DOI: 10.2140/jomms.2006.1.3

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Isogeometric Shell Analysis - Isogeometric Analysis

Isogeometric Analysis⁴ bridges Computer Aided Design (CAD) and Finite Element Analysis (FEA) by employing the same ('*iso*') functions for the representation of the geometry and solutions.

$$\mathcal{S}(\xi,\eta) = \sum_{i,j} \mathsf{C}_{ij} \varphi_{ij}(\xi,\eta)$$



"Let no man ignorant of geometry enter here." 5

⁵ J. A. Cottrell et al. (2009). Isogeometric Analysis: Toward Integration of CAD and FEA. Wiley, pp. 1–335. ISBN: 9780470748732. DOI: 10.1002/9780470749081

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⁴T. Hughes et al. (2005). "Isogeometric analysis: CAD, finite elements, NURBS, exact geometry and mesh refinement". In: Comput. Methods Appl. Mech. Eng. 194.39-41, pp. 4135-4195

Isogeometric Shell Analysis - Isogeometric Analysis





Multi-Patch surface $\mathcal{S} = \bigcup_i \mathcal{S}_i$

Control Net, $C_k = \bigcup_{ij} C_{ij}$ of patches \mathcal{S}_k , k = 0, 1, ...



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Isogeometric Shell Analysis - Isogeometric Kirchhoff-Love Shell

Definition (Kirchhoff Hypothesis)

In the Kirchhoff hypothesis, the following is assumed

- Straight lines perpendicular to the mid-plane before deformation remain perpendicular to the mid-surface after deformation;
- The normals rotate such that they remain perpendicular to the mid-surface after deformation;
- 3 The normals do not experience elongation (i.e. they are inextensible).



Isogeometric Shell Analysis - Variational Formulation

Variational formulation⁶

Find $u \in \mathcal{V}$ s.t.

$$\mathcal{N}(\mathsf{u},\phi) = \int_{\Omega} \boldsymbol{n}(\mathsf{u}) : \boldsymbol{\varepsilon}'(\mathsf{u},\phi) + \boldsymbol{m}(\mathsf{u}) : \boldsymbol{\kappa}'(\mathsf{u},\phi) \,\mathrm{d}\Omega - \int_{\Omega} \mathsf{f}(\mathsf{u}) \cdot \phi \,\mathrm{d}\Omega = \mathbf{0} \quad \forall \phi \in \mathcal{V}$$

With $\mathbf{n} = n^{\alpha\beta} \mathring{g}_{\alpha} \otimes \mathring{g}_{\beta}$ and $\mathbf{m} = m^{\alpha\beta} \mathring{g}_{\alpha} \otimes \mathring{g}_{\beta}$ the membrane force and bending moment tensors,

$$n^{\alpha\beta} = \int_{[-t/2,t/2]} S^{\alpha\beta} \,\mathrm{d}\theta_3 \qquad \qquad m^{\alpha\beta} = \int_{[-t/2,t/2]} \theta_3 S^{\alpha\beta} \,\mathrm{d}\theta_3$$

With $S^{\alpha\beta}$ the stress tensor depending on the (un)deformed geometry $\mathring{S}(S)$, containing linear, hyperelastic ⁷ or other constitutive models.

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⁶J. Kiendl et al. (2009). "Isogeometric shell analysis with Kirchhoff–Love elements". In: Computer Methods in Applied Mechanics and Engineering 198.49-52, pp. 3902–3914. ISSN: 0045-7825. DOI: 10.1016/J.CMA.2009.08.013

⁷ J. Kiendl et al. (2015). "Isogeometric collocation methods for the Reissner-Mindlin plate problem". In: Computer Methods in Applied Mechanics and Engineering 284, pp. 489–507. ISSN: 0045-7825. DOI: 10.1016/J.CMA.2014.09.011; Verhelst, H.M. et al. (2021). "Strend-Based Hyperelastic Material Formulations for Isogeometric Kirchhoff-Love Shells with Application to Winkling". In: Computer-Aided Design 139, p. 10375. ISSN: 0104485. DOI: 10.1016/J.cad.2021.103075

Isogeometric Shell Analysis - Isogeometric Kirchhoff-Love Shell



Collapse of a shallow roof. Left: solution + control points; middle: solution; right: control points



+ Geometric exactness

- + k-refinement (i.e. arbitrary smoothness across elements)
- -/- No rotational degrees of freedom; but requires C^1 smooth (i.e. quadratic) basis
 - Higher smoothness \implies bigger band-with in (stiffness) matrix

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Isogeometric Shell Analysis - Smooth Multi-Patch Analysis

Requirements

The curvature term in the variational formulation requires C_1 -smoothness everywhere; also on patch boundaries.

- Mortar-based methods ⁸
- Weak coupling methods (e.g. penalty, Nitsche) ⁹
- Strong coupling methods, e.g. D-Patch, Almost-C₁, Approximate-C₁, Exact-C₁¹⁰

⁸Horger et al. 2019; Dornisch et al. 2015

⁹Guo et al. 2019; Coox et al. 2017; Liu et al. 2019; Herrema et al. 2019; "Coupling of non-conforming trimmed isogeometric Kirchhoff-Love shells via a projected super-penalty approach"; Leonetti et al. 2020; Zhao et al. 2022

¹⁰Verhelst, H.M. et al. In preparation(b); Toshniwal et al. 2017; Takacs et al. 2022; Weinmüller et al. 2021; Farahat et al. In preparation

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Arc-Length Methods

Find $G(u, \lambda) = 0$ by steps constrained by equation $f(\Delta u, \Delta \lambda)$

- **1** Start at (u_i, λ_i) , $G(u_i, \lambda_i) = 0$
- **2** Find $\Delta(u_i, \Delta \lambda_i)$ s.t. $G(u_i, \lambda_i) = 0$ and $f(\Delta u, \Delta \lambda) = 0$

 $(\mathbf{u}_{i+1}, \lambda_{i+1}) = \\ (\mathbf{u}_i, \lambda_i) + \Delta(\mathbf{u}_i, \Delta\lambda_i)$

• Set i = i + 1 and go to 1



Arc-Length Methods

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- 4 Set i = i + 1 and go to 1



Path-Following Methods - Within-Branch Parallelization

Parallel Adaptive ALM ¹¹

 Compute coarse approximation of the path



\bullet = Main; \bullet = Worker;

¹¹Verhelst, H.M. et al. (In preparation[a]). "An Adaptive Parallel Arc-Length Method".

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Parallel Adaptive ALM ¹¹

- Compute coarse approximation of the path
- 2 Map the coarse approximation on a parametric domain $\xi \in [0, 1]$



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Parallel Adaptive ALM ¹¹

- Compute coarse approximation of the path
- Map the coarse approximation on a parametric domain $\xi \in [0, 1]$
- ③ Perform fine steps in each coarse subdomain



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Parallel Adaptive ALM 11

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Parallel Adaptive ALM 11

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- Check the distance between the fine and coarse approximation (using f(Δu, Δλ))
- **(3)** if $\varepsilon < \text{TOL}$: Rescale and mark



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Parallel Adaptive ALM¹¹

- 1 Compute coarse approximation of the path
- Map the coarse approximation on a parametric domain $\xi \in [0, 1]$
- Or Perform fine steps in each coarse subdomain
- Check the distance between the fine and coarse approximation (using $f(\Delta u, \Delta \lambda)$)
- **G** if $\varepsilon < \text{TOL}$: Rescale and mark
- 6 Go to 2 for marked segments
- \bullet = Main; \bullet = Worker:

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¹¹Verhelst, H.M. et al. (In preparation[a]), "An Adaptive Parallel Arc-Length Method".



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Effect of initial perturbations to avoid passing bifurcation points.



Arc-Length Method without perturbations





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Arc-Length Method without perturbations





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Effect of initial perturbations to avoid passing bifurcation points.



Arc-Length Method without perturbations



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Given Bifurcation detection, in addition to bifurcation tangents, multiple branches can be explored in parallel 12



¹² J. Thies et al. (2021). "Towards Scalable Automatic Exploration of Bifurcation Diagrams for Large-Scale Applications". In: Lecture Notes in Computational Science and Engineering 139, pp. 981–989. ISSN: 21977100. DOI: 10.1007/978-3-030-55874-1_97/FIGURES/5

Given Bifurcation detection, in addition to bifurcation tangents, multiple branches can be explored in parallel¹²



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Results - Shear Wrinkling





Experimental results¹³.

13W. Wong et al. (2006). "Wrinkled membranes I: experiments". In: Journal of Mechanics of Materials and Structures 1.1, pp. 3–25. ISSN: 1559-3959. DOI: 10.2140/jomms.2006.1.3

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Conclusions and Future Work - Conclusions

 Wrinkling occurs when in membrane-like¹⁴ offshore solar platforms; hence (isogeometric) shell modelling is used

- Isogeometric Kirchhoff-Love shells require C¹-smoothness across patch interfaces, but...
- Provide geometric exactness, arbitrary smoothness in a rotation-free setting.
- Wrinkling is a buckling instability, hence continuation methods are important
 - Continuation without a priori perturbations provides robustness, and...
 - Enables automatic exploration for subsequent bifurcations
 - Paralellization in continuation methods can be performed across and within branches

 $^{^{14}}$ With finite bending stiffness because of the energy balance!

Conclusions and Future Work - Conclusions

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Conclusions and Future Work - Future Work



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Geometry + Simulation Modules (G+SMo, pronounced gismo)

YES! 👌

lsogeometric analysis core github.com/gismo/gismo
Thin shell analysis github.com/gismo/gsKLShell
Arc-length methods github.com/gismo/gsStructuralAnalysis
Almost

Smooth patch coupling

github.com/gismo/gsUnstructuredSplines, expected Summer 2022





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Automatic exploration PyNCT, expected fall 2022



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